Short on the Q-system

The *Q-system* for rock mass classification, developed at the Norwegian Geotechnical Institute (NGI) in 1974, originally included a little more than 200 tunnel case histories, mainly from Scandinavia (Barton et al., 1974). In 1993 the system was updated to include more than 1000 cases (Grimstad and Barton, 1993). It is a quantitative classification system for estimates of tunnel support, based on a numerical assessment of the rock mass quality using the following six parameters:

- Rock quality designation (RQD).
- Number of joint sets (J_n).
- Roughness of the most unfavourable joint or discontinuity (J_r).
- Degree of alteration or filling along the weakest joint (J_a).
- Water inflow (J_w).
- Stress condition given as the stress reduction factor (SRF); composed of
 - Loosening load in the case of shear zones and clay bearing rock,
 - Rock stress in competent rock, and
 - Squeezing and swelling loads in plastic, incompetent rock.

The above six parameters are grouped into three quotients to give the overall rock mass quality:

$$Q = \frac{RQD}{J_n} \times \frac{J_r}{J_a} \times \frac{J_w}{SRF}$$

- The first two parameters represent the overall structure of the rock mass, and their quotient is a relative measure of the block size.
- The second quotient is described as an indicator of the inter-block shear strength.
- The third quotient is described as the "active stresses".

The ratings of the various input parameters to the Q-value are given in Table 1.

The Q-value is related to tunnel support requirement by defining the equivalent dimensions of the underground opening. This equivalent dimension, which is a function of the size and type of the excavation, is obtained by dividing the span, diameter or wall height of the excavation (Dt) by a quantity called the *excavation support ratio (ESR)*, given as:

$$De = \frac{Dt}{ESR}$$

Ratings of ESR are shown in Table 2

The Q-value in Figure 1 is related to the total amount of support (temporary and permanent) in the roof. The diagram is based on numerous tunnel support cases. Wall support can also be found using the same figure by applying the wall height and the following adjustments to Q:

$$\begin{array}{lll} For & Q > 10 & & use & Q_{wall} = 5Q \\ For & 0.1 < Q < 10 & & use & Q_{wall} = 2.5Q \\ For & Q < 0.1 & & use & Q_{wall} = Q \end{array}$$

Table 1. Description and ratings for the input parameters of the Q-system (simplified from Grimstad and Barton, 1993).

RQD (Rock Quality Designation)

Very poor	RQD = 0 - 25%
Poor	25 - 50
Fair	50 - 75
Good	75 - 90
Excellent	90 - 100
Notes:	

(i) Where RQD is reported or measured as < 10 (including 0), a nominal value of 10 is used to evaluate Q

(ii) RQD intervals of 5, i.e. 100, 95, 90, etc. are sufficiently accurate

Jn (joint set number)

Massive, no or few joints	Jn = 0.5 - 1	
One joint set	2	
One joint set plus random joints	3	
Two joint sets	4	
Two joint sets plus random joints	6	
Three joint sets	9	
Three joint sets plus random joints	12	
Four or more joint sets, heavily jointed, "sugar-cube", etc.	15	
Crushed rock, earthlike	20	
Notes: (i) For tunnel intersections, use (3.0 x Jn); (ii) For portals, use (2.0 x Jn)		

Jr (joint roughness number)

a) Rock-wall contact,					
b) rock-wall contact before 10 cm shear		c) No rock-wall contact when sheared			
Discontinuous joints	Jr = 4	Zone containing clay minerals thick enough to prevent rock-	Jr = 1.0		
Rough or irregular, undulating	3	wall contact	JI = 1.0		
Smooth, undulating	2	Sandy, gravelly or crushed zone thick enough to prevent rock-	1.0		
Slickensided, undulating	1.5	wall contact	1.0		
Rough or irregular, planar	1.5	Notes:			
Smooth, planar	1.0	i) Add 1.0 if the mean spacing of the relevant joint set is greater than 3 m			
Slickensided, planar	0.5	ii) Jr = 0.5 can be used for planar, slickensided joints having lineations,			
Note: i) Descriptions refer to small scale features,		provided the lineations are oriented for minimum strength			
and intermediate scale features, in that order					

Ja (joint alteration number)

0 00 () 0	ou (joint attoration nambor)					
en	JOINT WALL CHARACTER		Condition		Wall contact	
between walls		Healed or welded joints:		filling of quartz, epidote, etc.		Ja = 0.75
betwe	CLEAN JOINTS	Fresh joir	nt walls:	no coating or filling, except from sta	aining (rust)	1
		Slightly a	Itered joint walls: non-softening mineral coatings, clay-free particles, etc.		2	
ontact joint	COATING OR THIN	Friction n	naterials:	sand, silt, calcite, etc. (non-softening)		3
ပိ	S FILLING Cohesi		materials:	clay, chlorite, talc, etc. (softening)		4
wall					Some wall contact	No wall contact
	FILLING O	F:		Туре	Thin filling (< 5 mm)	Thick filling
ie or no contact	Friction materials		sand, silt calcite, etc. (non-softening)		Ja = 4	Ja = 8
e or	Hard cohesive mate	erials	compacted filling of clay, chlorite, talc, etc.		6	5 - 10
Some	Soft cohesive mate	erials medium to low		medium to low overconsolidated clay, chlorite, talc,		12
ο̈	Swelling clay materials		filling material exhibits swelling properties		8 - 12	13 - 20

Jw (joint water reduction factor)

Dry excavations or minor inflow, i.e. < 5 l/min locally	$p_w < 1 \text{ kg/cm}^2$	Jw = 1			
Medium inflow or pressure, occasional outwash of joint fillings	1 - 2.5	0.66			
Large inflow or high pressure in competent rock with unfilled joints	2.5 - 10	0.5			
Large inflow or high pressure, considerable outwash of joint fillings	2.5 - 10	0.3			
Exceptionally high inflow or water pressure at blasting, decaying with time	> 10	0.2 - 0.1			
Exceptionally high inflow or water pressure continuing without noticeable decay	> 10	0.1 - 0.05			
Note: (i) The last four factors are crude estimates. Increase Jw if drainage measures are installed					
(ii) Special problems caused by ice formation are not considered					

SRF (Stress Reduction Factor)

presence of water

rock

SRF (Stre	ss Reduction Factor)				
Multiple weakness zones with clay or chemically disintegrated rock, very loose surrounding rock (any depth)					
Multiple weakness zones with clay or chemically disintegrated rock, very loose surrounding Single weakness zones containing clay or chemically disintegrated rock (depth of excavation of the containing clay or chemically disintegrated rock (depth of excavation of the containing clay or chemically disintegrated rock).					5
	Single weakness zones containing clay or	ation > 50 m)		2.5	
Single weakness zones containing clay or chemically disintegrated rock (depth of excavation < 50 m) Single weakness zones containing clay or chemically disintegrated rock (depth of excavation > 50 m) Multiple shear zones in competent rock (clay-free), loose surrounding rock (any depth) Single shear zones in competent rock (clay-free), loose surrounding rock (depth of excavation < 50 m) Single shear zones in competent rock (clay-free), loose surrounding rock (depth of excavation < 50 m)					7.5
Single shear zones in competent rock (clay-free), loose surrounding rock (depth of excavation < 50 m)					5
Vea ir	Single shear zones in competent rock (clay-free), loose surrounding rock (depth of excavation > 50 m)				
>	Loose, open joints, heavily jointed or "sugar-cube", etc. (any depth)				5
Note: (i) Reduce these SRF values by 25 - 50% if the relevant shear zones only influence, but do not intersect the excavation.					
			$\sigma_{\rm c}/\sigma_{\rm 1}$	$\sigma_{\theta} / \sigma_{c}$	SRF
X,	Low stress, near surface, open joints		> 200	< 0.01	2.5
Low stress, near surface, open joints Survey Medium stress, favourable stress condition				0.01 - 0.3	1
Competent rock stre problem	Medium stress, favourable stress condition High stress, very tight structure. Usually favourable to stability, may be except for walls Moderate slabbing after > 1 hour in massive rock Slabbing and rock burst after a few minutes in massive rock				0.5 - 2
oete Sk s rob	Moderate slabbing after > 1 hour in massive rock 5 - 3				5 - 50
7 P	Slabbing and rock burst after a few minute	3 - 2	0.65 - 1	50 - 200	
ပိ	Heavy rock burst (strain burst) and immed	nd immediate dynamic deformation in massive rock < 2 >			200 - 400
Notes: (ii) Fo	or strongly anisotropic stress field (if measured): v	when 5 < $\sigma_{\rm 1}/\sigma_{\rm 3}$ <10, reduce $\sigma_{\rm c}$ to 0.75 $\sigma_{\rm c}$. When $\sigma_{\rm c}$	$1/\sigma 3 > 10$,	reduce σ_c t	o 0.5 σ_c
(iii) Few case records available where depth of crown below surface is less than span width. Suggest SRF increase from 2.5 to 5 for low stress					s cases
				$\sigma_{\theta} / \sigma_{c}$	SRF
Squeezing Plastic flow of incompetent rock under Mild squeezing rock pressure 1 - 5		1 - 5	5 - 10		
rock	rock the influence of high pressure Heavy squeezing rock pressure > 5		> 5	10 - 20	
Swelling	Iling Chemical swelling activity depending on Mild swelling rock pressure			5 - 10	

Heavy swelling rock pressure

Table 2 Ratings of the excavation support ratio (ESR) (from Barton et. al., 1974).

Type or use of underground opening	ESR
Temporary mine openings	3.5
Vertical shafts, rectangular and circular respectively	2.0 - 2.5
Water tunnels, permanent mine openings, adits, drifts	1.6
Storage caverns, road tunnels with little traffic, access tunnels, etc.	1.3
Power stations, road and railway tunnels with heavy traffic, civil defence shelters, etc.	1.0
Nuclear power plants, railroad stations, sport arenas, etc.	0.8

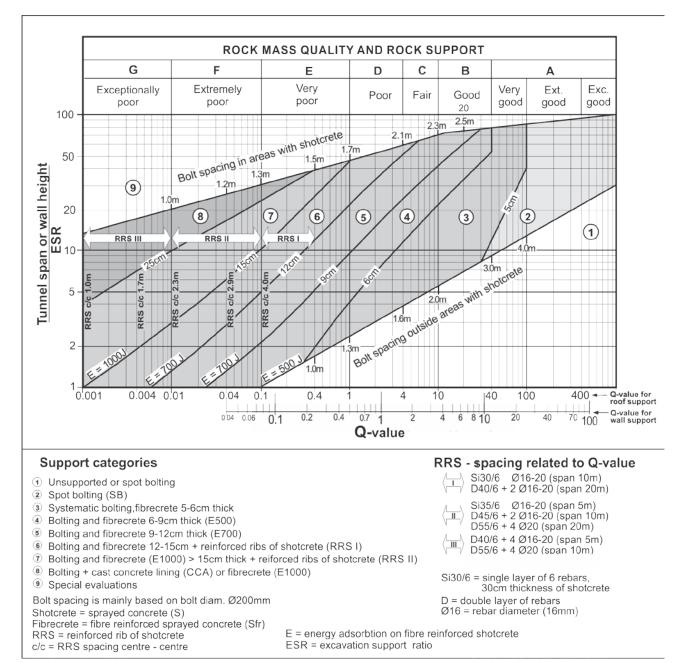


Figure 1 The Q system chart for rock support estimate, developed by the Norwegian Geotechnical Institute (NGI), (based on www.ngi.no, 2014). The Qwall values have been introduced in the chart